

The Advanced Spacecraft Propulsion and Energy Laboratory

Hyperion-I Phase I: Single Channel Test Readiness Review

Sam Cendro | Trey Cranney | Diego Ochoa-Cota | Branden Kretschmer



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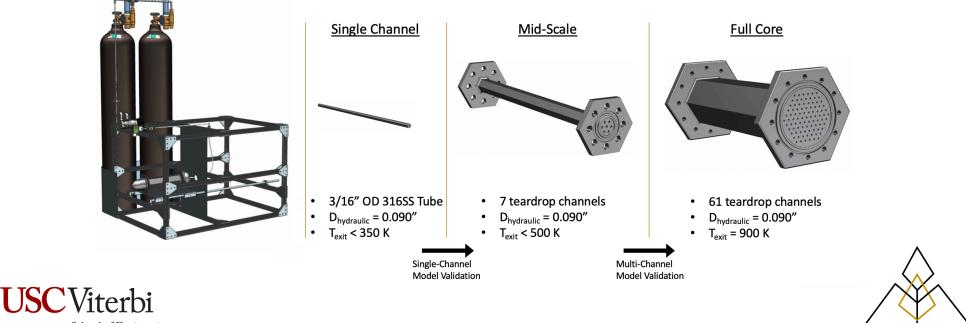
Phase I Completion





Hyperion-I Campaign Overview

- First engine modeling a solid core nuclear thermal rocket engine
- Additively manufactured metallic core
- Three Phases



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Phase I Overview

Goal: Characterize Heating Behavior

3/16" OD 316 SS tube

- Measure:
 - Propellant ΔT from inlet to outlet
 - Maximum metal temperature
 - Propellant $\Delta \mathsf{P}$ from inlet to outlet







Phase I Overview

Comparison to Model Results

- ANSYS multiphysics simulations
 - Maxwell
 - Fluent
 - Steady-State Thermal
 - Transient Thermal
- Phase I experimental results will determine if model needs to be refined for Phases II and III

- Model Setup:
 - T_{inlet} = 300 K
 - P_{inlet} = 500 psig
- Model Predictions:
 - T_{exit} = 339.75 K
 - T_{metal,max} ≈ 400 K
 - ΔT = 39.75 K



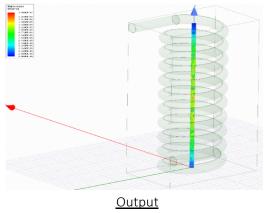


Phase I Overview

Multiphysics Model Structure

Electromagnetic

- ANSYS Maxwell 3D
- Input current limited by in-house induction heater

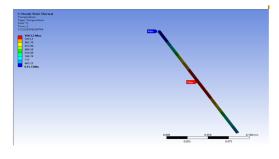


Ohmic loss contour



<u>Thermal</u>

- ANSYS Transient + Steady State Thermal
- Volumetric heating conditions imported via Maxwell ohmic loss map
- Ambient convection conditions assigned for dry heating tests



<u>Outputs</u>

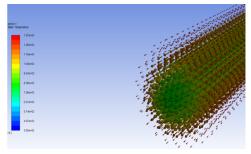
• Transient and steady state temperature maps of test article heating without working fluid flow conditions



ANSYS FLUENT

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- Imports ohmic losses from Maxwell
 model
- Working fluid pressures assigned at inlet and outlet mesh boundaries
- Assumes thermally insulated test articles



<u>Outputs</u>

- Working fluid outlet conditions
- Steady state test article temperature

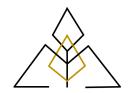


Design Approach

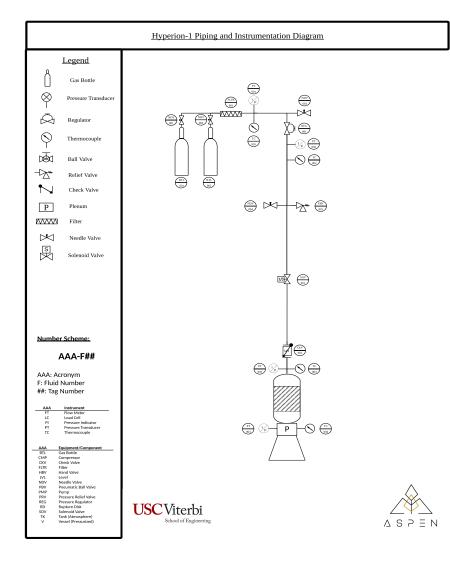
Test Stand Requirements:

- Flow gaseous nitrogen at a rate of up to 0.11 lb/s (90.4 SCFM , 0.05 kg/s)
- •Supply nozzle inlet with nitrogen up to 1000 psig
- Supply pressurized nitrogen flow for a total time of 15 min
- •Acquire data for temperature, pressure, and thrust throughout system
- •Able to relieve the system from high pressures to keep personnel and crucial components safe
- Phase I test requirements will also be discussed
 - Pressure: 500 psig
 - Flow rate: 0.00025kg/s





P&ID







Line Sizing

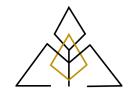
- Conditions:
 - Gas Nitrogen
 - Pressure 1000 psig
 - Flow Rate 0.11 lb/s (0.05 kg/s)

•¼" line was chosen for facilitated routing and lower-cost components

•5 ft of ¼" line, total pressure drop is 45 psig across the system.

Line Size [in]	Pressure Drop [psi/ft]
1"	0.003
3/4"	0.01
1/2"	0.12
3/8"	0.51
1/4"	8.00
1/8"	1200





Pressure Regulator

Requirement:

• 1000 psig at exit plenum and flow rate of 90.4 SCFM

Tescom 44-1300 Series

- • $C_v = 0.8$
- Max Inlet Pressure : 3500 psig
- Max Outlet Pressure : 1500 psig







Tescom 44-1300 Flow Curves

Flow Conditions:

- •2640 Inlet Pressure
- •1000 Outlet Pressure

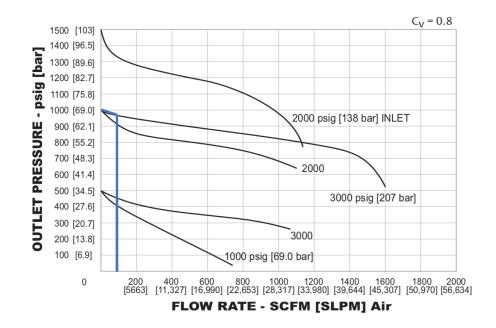
Flow Results:

- Flow Rate: 90.4 SCFM
- •Pressure Droop: ~ 40 psig
- •Regulator is able to produce desired flow

Phase 1 Conditions

- 2640 Inlet Pressure
- 500 Outlet Pressure
- Flow Rate: 0.45 SCFM
- Flow curves out of test conditions range, expecting minimal pressure droop.







Instrumentation

- Pressure Transducers:
 - •Omega PX309-3KG5V
 - •0 to 3000 psig
 - •Accuracy: 0.5 %
 - •¼″ NPT
- •Thermocouples:
 - •K-Type Omega KMQXL
 - •Max Temp: 2440 °F (Exit Plenum Temp: 1340 °F)
 - •¼'' Diameter
- •Load Cell
 - •Omega Thin Beam Load Cell LCL-040
 - •Low Range Capacity: 0 40 lb (170 N)





Mass Flow Measurement (Phase 1 & 2)

Calculated orifice size with choked flow equation for a compressible fluid

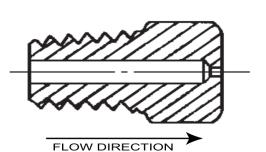
- $d = 9.62 \times 10^{-9} m = 0.01 in$
- $P_0 = 500 \ psi = 3346025.7 \ Pa$
- $C_d = 0.61$ (Sharp Edge Orifice)
- Nitrogen Properties:

•
$$\gamma = 1.4$$

- ρ = 39.72 kg/m³
 A = 7.27 x 10⁹ m²
- $\dot{m} = 0.00025 \frac{kg}{r}$

O'Keefe Controls Co. EM-10-BR Orifice

- 0.01" Outlet
- Max Pressure: 4000 psi





$$\dot{m}=C_{d}A\sqrt{\gamma
ho_{0}P_{0}igg(rac{2}{\gamma+1}igg)^{rac{\gamma+1}{\gamma-1}}}$$

Mass Flow Measurement (Phase III)

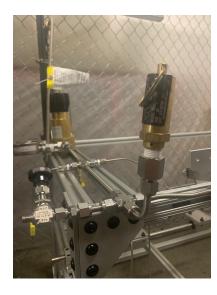
• Ideal gas flow through rocket nozzle equation:

$$\dot{m} = A_t P_0 \sqrt{g \gamma \left(\frac{2}{\gamma + 1}\right)^{\frac{\gamma + 1}{\gamma - 1}} / RT}$$

- *A_t*, Nozzle throat area
- *P*₀, upstream pressure
- *g*, gravitational constant
- *γ*, specific heat ratio
- *R*, gas constant
- *T*, total temperature

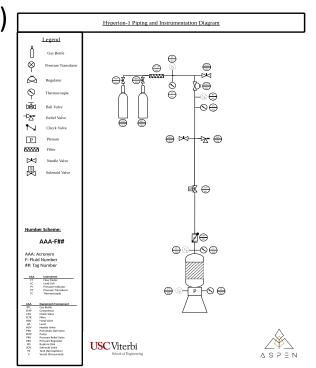
Post Feed System Peer Design Review (Dec. 7th, 2018)

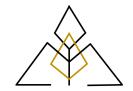
- Orientation of solenoid valve was changed to an upright position
- Relief valve positioned with the relief side facing up



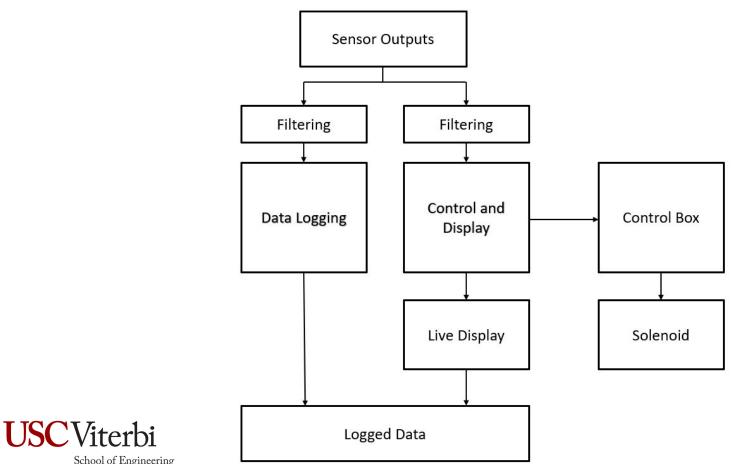








DAQ Overview





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DAQ Overview

DAQ Capabilities

ASPEN selected the Texas Instruments MSP432P401R for logging and control systems

Hardware Capacity Per Board:

- SAR Precision ADC with 16-bit performance
- 48MHz 32-bit ARM Cortex
- Memory: 256KB Flash, 64KB RAM
- Communication: Up to 4 I2C, 8 SPI, 4 UART

Overall Hardware Capacity:

- 9 current inputs/ 14 total possible
- 600Hz logging rate
- 12kHz Low pass filtering
- Onboard 12V low noise power supply
- 2 current solenoid control outputs/ 4 total possible
- Modular design, allows for easy and cheap board swapping for rapid iteration

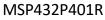
Software Capacity:

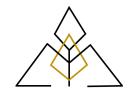
- Backend based in python, allows for multiprocessing and subprocess generation
- Embedded systems based in C



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DAQ Overview

Current Status

Hardware:

- 4 Thermocouples/4 Pressure Transducers Wired, Ninth input left open
- Two MSP432P401R boards installed with input shields attached
- Power supply Installed
- Inputs and shielding installed

Software:

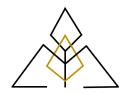
- Logging and Control scripts are running
- Live display running

Challenges Still to Finish:

- Live graphing has slight delay to new data being displayed
- Automated testing in still in the works
- 60Hz resonance is present, working on grounding shielding
- Resolve PT calibration offset errors







General Overview

- Completion necessary before commencing Hot Flow testing
- Ensures that the feed system and its components will hold pressure at the Maximum Expected Operating Pressure and to pressures exceeding this (Proof Pressure)
- Single Qualification Test:
 - Gas Leak/Proof with gaseous nitrogen





Safety and Certifications

- General Lab Safety Training
- Pressurized System Briefing for all Testing Technicians
- Test stand sandbagged in place

	Safety glasses
Required	Long pants
PPE	Closed-toe shoes
	Ear plugs





Operations

- Hot Work Permit for RRB Loading Dock
 - Good for one year
- Ordered both gaseous nitrogen tanks (size K) three days in advance
 - Readily available from USC facilities
 - Delivered to AME Offices in RRB 101
 - \$13 per month for each bottle





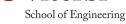




Operations

- Three primary roles during testing
 - Test Director
 - Test operation authority
 - Approves and directs procedural steps
 - DAQ Operator
 - Runs data acquisition program and actuates valves
 - Monitors leak rate during Leak Test and watches for unusual pressures
 - Technician
 - Operates pressure regulator and find leaks using snoop during Leak Test
 - Tightens any loose fittings





Gas Leak/Proof Testing

- Ensures all lines and fittings will hold pressure up to:
 - Maximum Expected Operating Pressure (MEOP) : 500 psig
 - Proof Pressure (MEOP*1.5) : 750 psig
- Pressure increased incrementally in Stages
- Feed system isolated in sections starting with component closest to the pressure regulator and moving downstream
- Pressure held at each stage for 3 min
- Leak Rate calculated at each Stage
- System considered proofed when Stage 4 is achieved

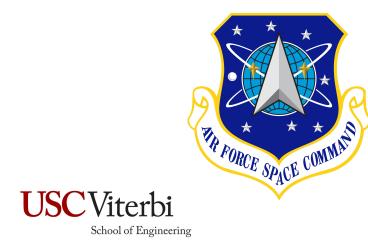
MEOP	500 psig
Leak Pressure (1.2*MEOP)	600 psig
Proof Pressure (1.5*MEOP)	750 psig
Stage 1	200 psig
Stage 2	400 psig
Stage 3	600 psig
Stage 4	750 psig



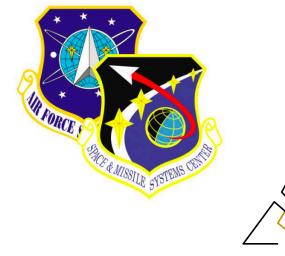


References

- HQ Air Force Space Command Guidance Memorandum for AFSPCMAN 91-710 Volume 6
- NASA Technical Standard: Leak Test Requirements. NASA-STD-7012. 2019.
- Space and Missile Systems Center Standard: Evaluation and Test Requirements for Liquid Rocket Engines. SMC Standard SMC-S-025.







Qualification Criterion

- Visual leak observance with snoop during section isolation at each Stage
 - If leaks are present, system is fully depressurized and leaky fittings are tightened
- Leak rate < 3 psig/min at each Stage
 - If leak rate over 3 psig/min then test restarts at Stage 1
 - 3 psig/min leak rate obtained from LPL's November 27th, 2018 Ox-line leak test





Attempt 1

- Test aborted due to scratched T-fitting upstream of the pressure regulator
 - Caused leakage
 - No extra part in lab, so a new one had to be ordered







Attempt 2

Note: Solenoid orientation was switched prior to leak checks

Parameter	Limit
Stage Pressure	200 psig
Max Pressure Reached	210 psig
Average Leak Rate	-0.66 psig/min

Parameter	Limit
Stage Pressure	600 psig
Max Pressure Reached	618 psig
Average Leak Rate	2.72 psig/min

Parameter	Limit
Stage Pressure	400 psig
Max Pressure Reached	388 psig
Average Leak Rate	-1 psig/min

Parameter	Limit
Stage Pressure	750 psig
Max Pressure Reached	762 psig
Average Leak Rate	1.21 psig/min





Lessons Learned & Feedback Received Post-Testing

- Need a cart to carry DAQ and organize wires
- Relief valve should be below Proof Pressure (750 psig)
 - During Leak/Proof it should be plugged somehow...





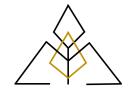


General Overview

- Purpose of obtaining temperature and pressure measurements to compare against ANSYS Multiphysics model results
- ANSYS model predicts ~10 min for dry heating steady state thermal
 - Used to determine experiment run time
- Heater turned on upon opening of the primary solenoid

Operating Pressure	500 psig
Heater Setting	300 A
Testing Period 10 mi	

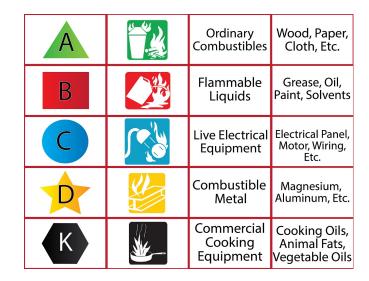


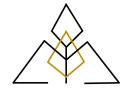


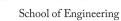
Safety and Certifications

- General Lab Safety Training
- Pressurized System Briefing for all Testing Technicians
- USC EH&S General Lab Safety Training
- Class A and Class C Fire Extinguisher available
- Faraday cage for electromagnetic radiation containment
- Fire Department notified of testing
- Cones set up around Loading Dock and sidewalk
- Test stand and cylinders sandbagged in place

	Safety glasses
Required	Long pants
PPF	Closed-toe shoes
	Ear plugs







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Operations

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 - Approves and directs procedural steps.
 - Depressurizes system
 - DAQ Operator
 - Runs data acquisition program and actuates valves
 - Watches for unusual pressures and other anomalies in the data
 - Technician
 - Sets heater to proper amperage
 - Sets regulator to operating pressure

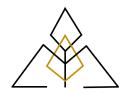




Refinements to Operations after Leak/Proof Testing

- Added a Crew Chief position upon Advisor recommendation
 - Oversee all testing operations are running smoothly and correctly
- Included additional gas cylinder safety and logistics information for more streamlined setup and disassembly
- Setup cones around the loading dock and adjacent sidewalk
- Include more emergency shutdown procedures
- Thermal Camera to continuously metal temp of single channel test article





Phase I Completion

- Comparison of DAQ experimental data to ANSYS multiphysics models
- White paper on results
- Presentation at NETS (Nuclear and Emerging Technologies for Space)
 - April 6-10 in Knoxville, Tennessee
 - Sponsored by Oakridge National Laboratory
- 2020 AIAA Propulsion and Energy Conference
 - August 24-26 in New Orleans, Louisiana
- Refine methodology for Phase II Hot Flow Testing











